

PCT

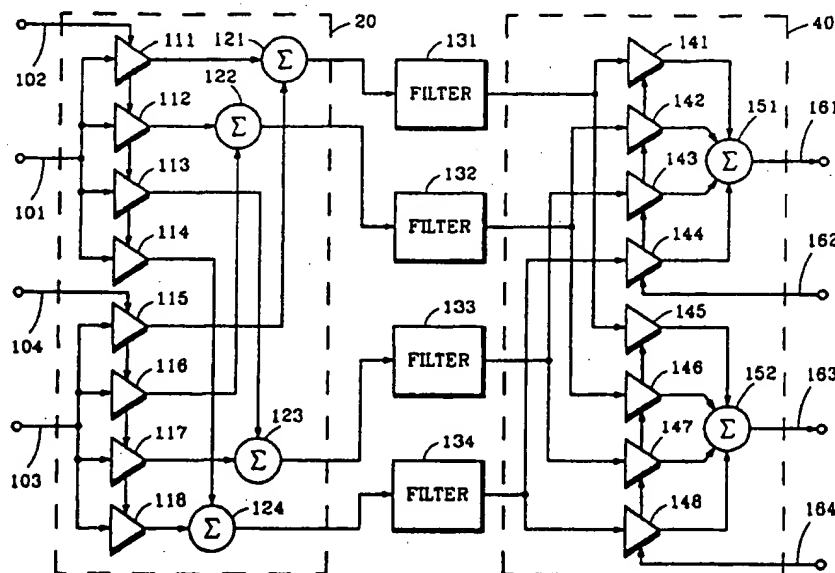
WORLD INTELLECTUAL PROPERTY ORGANIZATION
International Bureau



INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification 6: H04S 5/00	A1	(11) International Publication Number: WO 96/13962
		(43) International Publication Date: 9 May 1996 (09.05.96)
(21) International Application Number: PCT/US95/13874		(81) Designated States: AU, CA, JP, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).
(22) International Filing Date: 26 October 1995 (26.10.95)		
(30) Priority Data: 08/330,240 27 October 1994 (27.10.94) US		Published With international search report. Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.
(71) Applicant: CRYSTAL RIVER ENGINEERING, INC. [US/US]; Suite 200, 490 California Avenue, Palo Alto, CA 94306 (US).		
(72) Inventors: ABEL, Jonathan, S.; 184 Tennyson Avenue, Palo Alto, CA 94301 (US). FOSTER, Scott, H.; 12350 Wards Ferry Road, Groveland, CA 95321 (US).		
(74) Agents: GALLAGHER, Thomas, A. et al.; Law Offices of Thomas A. Gallagher, 3rd floor, 100 Green Street, San Francisco, CA 94111-1302 (US).		

(54) Title: METHOD AND APPARATUS FOR EFFICIENT PRESENTATION OF HIGH-QUALITY THREE-DIMENSIONAL AUDIO



(57) Abstract

Spatialization of soundfields is accomplished by filtering audio signals using filters having unvarying frequency response characteristics and amplifying signals using amplifier gains adapted in response to signals representing sound source location and/or listener position. The filters are derived using a singular value decomposition process which finds the best set of component impulse responses to approximate a given set of head related transfer functions. Efficient implementations for rendering reflection effects and for spatializing multiple sound sources and/or generating multiple output signals are disclosed.

FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AT	Austria	GB	United Kingdom	MR	Mauritania
AU	Australia	GE	Georgia	MW	Malawi
BB	Barbados	GN	Guinea	NE	Niger
BE	Belgium	GR	Greece	NL	Netherlands
BF	Burkina Faso	HU	Hungary	NO	Norway
BG	Bulgaria	IE	Ireland	NZ	New Zealand
BJ	Benin	IT	Italy	PL	Poland
BR	Brazil	JP	Japan	PT	Portugal
BY	Belarus	KE	Kenya	RO	Romania
CA	Canada	KG	Kyrgyzstan	RU	Russian Federation
CF	Central African Republic	KP	Democratic People's Republic of Korea	SD	Sudan
CG	Congo	KR	Republic of Korea	SE	Sweden
CH	Switzerland	KZ	Kazakhstan	SI	Slovenia
CJ	Côte d'Ivoire	LI	Liechtenstein	SK	Slovakia
CM	Cameroon	LK	Sri Lanka	SN	Senegal
CN	China	LU	Luxembourg	TD	Chad
CS	Czechoslovakia	LV	Latvia	TG	Togo
CZ	Czech Republic	MC	Monaco	TJ	Tajikistan
DE	Germany	MD	Republic of Moldova	TT	Trinidad and Tobago
DK	Denmark	MG	Madagascar	UA	Ukraine
ES	Spain	ML	Mali	US	United States of America
FI	Finland	MN	Mongolia	UZ	Uzbekistan
FR	France			VN	Viet Nam
GA	Gabon				

DESCRIPTION

METHOD AND APPARATUS FOR EFFICIENT PRESENTATION OF HIGH-QUALITY THREE-DIMENSIONAL AUDIO

Technical Field

5 The invention relates in general to the presentation of audio signals conveying an impression of a three-dimensional sound field and more particularly to an efficient method and apparatus for high-quality presentations.

Background

10 There is a growing interest to improve methods and systems for audio displays which can present audio signals conveying accurate impressions of three-dimensional sound fields. Such audio displays utilize techniques which model the transfer of acoustic energy in a soundfield from one point to another. A frequency-domain form of such models is referred to as an acoustic transfer function (ATF) and may be expressed as a function $H(d, \theta, \phi, \omega)$ of frequency ω and relative position (d, θ, ϕ) between two points, where (d, θ, ϕ) represents the relative position of the two points in polar coordinates. Other coordinate systems may be used.

15 Throughout the following discussion, more particular mention is made of various frequency-domain transfer functions; however, it should be understood that corresponding time-domain impulse response representations exist which may be expressed as a function of time t and relative position between points, or $h(d, \theta, \phi, t)$. The principles and concepts discussed here are applicable to either domain.

20 An ATF may model the acoustical properties of a test subject. In particular, an ATF which models the acoustical properties of a human torso, head, ear pinna and ear canal is referred to as a head-related transfer function (HRTF). A HRTF describes, with respect to a given individual, the acoustic levels and phases which occur near the ear drum in response to a given soundfield. The HRTF is typically a function of both frequency and relative orientation between the head and the source of the soundfield. A HRTF in the form of a free-field transfer function (FFTF) expresses changes in level and phase relative to the levels and phase which would exist if the test subject was not in the soundfield; therefore, a HRTF in the form of a FFTF may be generalized as a transfer function of the form $H(\theta, \phi, \omega)$. The effects of distance can usually be simulated by amplitude attenuation

25

30

proportional to the distance. In addition, high-frequency losses can be synthesized by various functions of distance. Throughout this discussion, the term HRTF and the like should be understood to refer to FFTF forms unless a contrary meaning is made clear by explanation or by context.

5 Many applications comprise acoustic displays utilizing one or more HRTF in attempting to "spatialize" or create a realistic three-dimensional aural impression. Acoustic displays can spatialize a sound by modelling the attenuation and delay of acoustic signals received at each ear as a function of frequency ω and apparent direction relative to head orientation (θ, ϕ) . An impression that an acoustic signal originates from a particular
10 relative direction (θ, ϕ) can be created in a binaural display by applying an appropriate HRTF to the acoustic signal, generating one signal for presentation to the left ear and a second signal for presentation to the right ear, each signal changed in a manner that results in the respective signal that would have been received at each ear had the signal actually originated from the desired relative direction.

15 Empirical evidence has shown that the human auditory system utilizes various cues to identify or "localize" the relative position of a sound source. The relationship between these cues and relative position are referred to here as listener "localization characteristics" and may be used to define HRTF. The differences in the amplitude and the time of arrival of soundwaves at the left and right ears, referred to as the interaural intensity difference
20 (IID) and the interaural time difference (ITD), respectively, provide important cues for localizing the azimuth or horizontal direction of a source. Spectral shaping and attenuation of the soundwave provides important cues used to localize elevation or vertical direction of a source, and to identify whether a source is in front of or in back of a listener.

 Although the type of cues used by nearly all listeners is similar, localization
25 characteristics differ. The precise way in which a soundwave is altered varies considerably from one individual to another because of considerable variation in the size and shape of human torsos, heads and ear pinnae. Under ideal situations, the HRTF incorporated into an acoustic display is the personal HRTF of the actual listener because a universal HRTF for all individuals does not exist. Additional information regarding the suitability of shared
30 HRTF may be obtained from Wightman, et al., "Multidimensional Scaling Analysis of Head-Related Transfer Functions," IEEE Workshop on Applications of Sig. Proc. to Audio and Acoust., October 1993.

 In many practical systems, however, several HRTF known to work well with a variety of individuals are compiled into a library to achieve a degree of sharing. The most

appropriate HRTF is selected for each listener. Additional information may be obtained from Wenzel, et al., "Localization Using Nonindividualized Head-Related Transfer Functions," J. Acoust. Soc. Am., vol. 94, July 1993, pp. 111-123.

The realism of an acoustic display can be enhanced by including ambient effects.

5 One important ambient effect is caused by reflections. In most environments, a soundfield comprises soundwaves arriving at a particular point, say at an ear, along a direct path from the sound source and along paths reflecting off one or more surfaces of walls, floor, ceiling and other objects. A soundwave arriving after reflecting off one surface is referred to as a first-order reflection. The order of the reflection increases by one for each additional
10 reflective surface along the path. The direction of arrival for a reflection is generally not the same as that of the direct-path soundwave and, because the propagation path of a reflected soundwave is longer than a direct-path soundwave, reflections arrive later. In addition, the amplitude and spectral content of a reflection will generally differ because of energy absorbing qualities of the reflective surfaces. The combination of high-order
15 reflections produces the diffuse soundfields associated with reverberation.

A HRTF may be constructed to model ambient affects; however, more flexible displays utilize HRTF which model only the direct-path response and include ambient effects synthetically. The effects of a reflection, for example, may be synthesized by applying a direct-path HRTF of appropriate direction to a delayed and filtered version of
20 the direct-path signal. The appropriate direction is the direction of arrival at the ear may be established by tracing the propagation path of the reflected soundwave. The delay accounts for the reflective path being longer than the direct path. The filtering alters the amplitude and spectrum of the delayed soundwave to account for acoustical properties of reflective surfaces, air absorption, nonuniform source radiation patterns and other
25 propagation effects. Thus, a HRTF is applied to synthesize each reflection included in the acoustic display.

In many acoustic displays, HRTF are implemented as digital filters. Considerable computational resources are required to implement accurate HRTF because they are very complex functions of direction and frequency. The implementation cost of a high-quality
30 display with accurate HRTF is roughly proportional to the complexity and number of filters used because the amount of computation required to perform the filters is significant as compared to the amount of computation required to perform all other functions. An efficient implementation of HRTF filters is needed to reduce implementation costs of high-quality acoustic displays. Efficiency is very important for practical displays of complex

- 4 -

soundfields which include many reflections. The complexity is essentially doubled in binaural displays and increases further for multiple sources and/or multiple listeners.

The term "filter" and the like as used here refer to devices which perform an operation equivalent to convolving a time-domain signal with an impulse response.

5 Similarly, the term "filtering" and the like as used here refer to processes which apply such a "filter" to a time-domain signal.

One technique used to increase the efficiency of spatializing late-arriving reflections is disclosed in U.S. patent 4,731,848. According to this technique, direct-path soundwaves and first-order reflections are processed in a manner similar to that discussed above. The
10 diffuse soundwaves produced by higher-order reflections are synthesized by a reverberation network prior to spectral shaping and delays provided by "directionalizers."

Another technique used to increase the efficiency of spatializing early reflections is disclosed in U.S. patent 4,817,149. According to this technique, three separate processes are used to spatialize the direct-path soundwave, early reflections and late reflections. The
15 direct-path soundwave is spatialized by providing front/back and elevation cues through spectral shaping, and is spatialized in azimuth by including either ITD or IID. The early reflections are spatialized by propagation delays and azimuth cues, either ITD or IID, and are spectrally shaped as a group to provide "focus" or a sense of spaciousness. The late reflections are spatialized in a manner similar to that done for early reflections except that
20 reverberation and randomized azimuth cues are used to synthesize a more diffuse soundfield.

These techniques improve the efficiency of spatializing reflections but they do not improve the efficiency of spatializing a direct-path soundwave nor do they provide a way to more efficiently spatialize binaural displays, to spatialize multiple sources or present a
25 spatialized display to multiple listeners.

A technique used to more efficiently spatialize an audio signal is implemented in the UltraSound™ multimedia sound card by Advanced Gravis Computer Technology Ltd., Burnaby, British Columbia, Canada. According to this technique, an initial process records several prefiltered versions of an audio signal. The prefiltered signals are obtained
30 by applying HRTF representing several positions, say four horizontal positions spaced apart by 90 degrees and one or two positions of specified elevation. Spatialization is accomplished by mixing the prefiltered signals. In effect, spatialization is accomplished by panning between fixed sound sources. The spatialization process is fairly efficient and has an intuitive appeal; however, it does not provide very good spatialization unless a fairly

- 5 -

large number of prefiltered signals are used. This is because each of the prefiltered signals include ITD, and a soundwave appearing to originate from an intermediate point cannot be reasonably approximated by a mix of prefiltered signals unless the signals represent directions fairly close to one another. Limited storage capacity usually restrict the number of prefiltered signals which can be stored. In addition, the technique imposes a rather serious disadvantage in that neither the HRTF nor the audio source can be changed without rerecording the prefiltered signals. This technique is described briefly in Begault, "3-D Sound for Virtual Reality and Multimedia," Academic Press, Inc., 1994, p. 210.

As explained above, accurate HRTF are expensive to implement because they are complex functions of direction and frequency. Research discussed in Martens, "Principal Components Analysis and Resynthesis of Spectral Cues to Perceived Direction," ICMC Proceedings, 1987, pp. 274-281, and in Kistler, et al., "A Model of Head-Related Transfer Functions Based on Principal Components Analysis and Minimum-Phase Reconstruction," J. Acoust. Soc. Am., March 1992, pp. 1637-1647, used principal component analysis to develop the concept that HRTF can be approximated fairly well by a small number of fixed-frequency-response basis functions. In particular, Kistler, et al. showed that as few as five log-magnitude basis functions could reasonably represent a direction-dependent portion of HRTF responses, referred to as directional transfer functions (DTF), for each ear of ten different test subjects. Direction-independent aspects such as ear canal resonance were excluded from the principal component analysis. Phase responses of the HRTF were approximated by ITD which were assumed to be frequency independent.

Kistler, et al. showed that binaural HRTF for a particular individual and specified direction can be approximated by scaling the log-magnitude basis functions with a set of weights, combining the scaled functions to obtain composite log-magnitude response functions representing DTF for each ear, deriving two minimum phase filters from the log-magnitude response functions, adding excluded direction-independent characteristics such as ear canal resonance to derive HRTF representations from the DTF representations, and calculating a delay for ITD to simulate phase response. Unfortunately, these basis functions do not provide for any improvement in implementation efficiency of HRTF. In addition, Kistler, et al. concluded that the principal component weights for the five basis functions were very complex functions of direction and could not be easily modeled.

There remains a need for a method to efficiently implement accurate HRTF, particularly for acoustic displays which spatialize multiple sources and/or generate unique displays for multiple listeners.

- 6 -

Disclosure of Invention

It is an object of the present invention to provide for a method and apparatus to efficiently implement accurate HRTF for high-quality acoustic displays.

5 It is another object of the present invention to provide for an efficient method and apparatus to spatialize multiple sources.

It is yet another object of the present invention to provide for an efficient method and apparatus to spatialize a source for binaural presentation to one or more listeners, for monaural presentation to two or more listeners, or for a combination of binaural and monaural presentations.

10 It is a further object of the present invention to provide for an efficient method and apparatus to spatialize multiple sources to multiple listeners, allowing for trade off between accuracy of spatialization and numbers of sources or listeners.

Other objects and advantages of the present invention may be appreciated by referring to the following discussion and to the accompanying drawings.

15 In accordance with the teachings of the present invention, a method or apparatus for providing an acoustic display comprises steps or means, respectively, for receiving an audio signal representing an acoustic source, receiving a location signal representing apparent location of the source, applying two or more filters to the audio signal, and generating a plurality of output signals by amplifying the output of each filter using
20 amplifier gains adapted in response to the location signal and combining the amplified signals. The output signals may provide binaural presentation to one or more listeners, monaural presentation to two or more listeners or a combination of binaural and monaural presentations.

In accordance with the teachings of the present invention, a method or apparatus for
25 providing an acoustic display comprises steps or means, respectively, for receiving audio signals representing two or more acoustic sources, receiving location signals representing apparent locations of the sources, amplifying each audio signal using amplifier gains adapted in response to the location signals, generating two or more intermediate signals by combining the amplified audio signals, applying two or more filters to the two or more
30 intermediate signals, and generating an output signal by combining the output of each filter.

In accordance with the teachings of the present invention, the method or apparatus just described may generate two or more output signals for binaural presentation to one or more listeners, monaural presentation to two or more listeners or a combination of binaural and monaural presentations by amplifying the output of each filter using amplifier gains

adapted in response to listener position and/or orientation and generating the two or more output signals by combining the amplified filtered signals.

In accordance with the teachings of the present invention, a method or apparatus for providing an acoustic display comprises steps or means, respectively, for receiving an audio signal representing an acoustic source, receiving a location signal representing apparent location of the source, rendering a direct-path response by applying a first filter with a frequency response adapted in response to the location signal, spatializing reflections by applying one or more second filters with unvarying frequency response to the audio signal and amplifying the output of each second filter using amplifier gain adapted in response to the location signal, and generating an output signal by combining signals passed by the first filter and the second filters. Alternatively, the steps of applying a second filter and amplifying with an adaptive gain may be interchanged.

Each of the methods and apparatuses in accordance with the present invention may be modified to also adapt the amplifier gains in response to listener position or personal localization characteristics. In preferred embodiments, one or more output signals are delayed in response to listener position, orientation and/or localization characteristics. The methods and apparatus may also adapt the amplifier gains and/or introduce delays in response to a signal representing ambient characteristics. High-quality displays may also filter and scale signals according to source aspect to account for nonuniform source radiation patterns and/or according to atmospheric and reflective-surface characteristics to account for transmission losses. Further, in some embodiments, amplifier gains may be adapted to provide for varying numbers of audio signals and/or output signals.

Throughout this discussion, references to binaural presentations should be understood to also refer to presentations utilizing more than two output signals unless the context of the discussion makes it clear that only a two-channel presentation is intended.

The present invention may be implemented in many different embodiments and incorporated into a wide variety of devices. It is contemplated that the present invention will be most frequently practiced using digital signal processing techniques implemented in software and/or so called firmware; however, the principles and teachings may be applied using other techniques and implementations. The various features of the present invention and its preferred embodiments may be better understood by referring to the following discussion and to the accompanying drawings in which like reference numbers refer to like features. The contents of the discussion and the drawings are provided as examples only

- 8 -

and should not be understood to represent limitations upon the scope of the present invention.

Brief Description of Drawings

Figure 1 is a functional block diagram illustrating one implementation of HRTF according to the present invention for use in an acoustic display for presentation of multiple sources in one output signal.

Figure 2 is a functional block diagram illustrating one implementation of HRTF according to the present invention for use in an acoustic display for presentation of a single source in multiple output signals.

Figure 3 is a functional block diagram illustrating one implementation of HRTF according to the present invention for use in an acoustic display for presentation of multiple sources in multiple output signals.

Figure 4 is a functional block diagram illustrating one implementation of a HRTF according to the present invention comprising a hybrid structure of filters with varying and unvarying frequency response characteristics.

Figure 5a-5b are functional block diagrams of filter-amplifier networks.

Figure 6 is a function block diagram illustrating one implementation of a HRTF according to the present invention comprising a hybrid structure of filters and an amplifier network in which a single set of filters with unvarying frequency response characteristics spatializes reflective effects for a single audio source and multiple output signals.

Figures 7a and 7b are functional block diagrams illustrating implementations of HRTF according to the present invention in which filters having unvarying frequency response characteristics were derived from impulse responses representing ATF such as directional transfer functions.

Modes for Carrying Out the Invention

Multiple Source Signals

A functional block diagram shown in Figure 1 illustrates one structure of a device according to the teachings of the present invention which implements HRTF for multiple audio sources. An audio signal representing a first audio source is received from path 101, amplified by a first group of amplifiers 111-114 and passed to combiners 121-124. Another audio signal representing a second audio source is received from path 103, amplified by a second group of amplifiers 115-118 and passed to combiners 121-124.

Combiner 121 combines amplified signals received from amplifiers 111 and 115 and passes the resulting intermediate signal to filter 131. Combiners 122-124 combine amplified signals received from other amplifiers as shown and pass the resulting intermediate signals to respective filters 132-134. Filters 131-134 each apply a filter to a respective
5 intermediate signal and pass the resulting filtered signals to combiner 151. Combiner 151 combines the filtered signals and passes the resulting output signal along path 161.

Location signals received from paths 102 and 104 represent the desired apparent locations of the sources of the audio signals received from paths 101 and 103, respectively. Respective gains of amplifiers 111-114 in the first group of amplifiers are adapted in
10 response to the location signal received from path 102 and respective gains of amplifiers 115-118 in the second group of amplifiers are adapted in response to the location signal received from path 104.

The structure shown in Figure 1 implements HRTF for two audio sources and can be extended to implement HRTF for additional sources by adding a group of amplifiers for each additional source and coupling the output of each amplifier in a group to a respective
15 combiner which is coupled to the input of a respective filter. The illustrated structure comprises four filters but as few as two filters may be used. Very accurate HRTF can generally be implemented using no more than twelve to sixteen filters.

Multiple Output Signals

20 A functional block diagram shown in Figure 2 illustrates one structure of a device according to the teachings of the present invention which implements HRTF for multiple output signals. Each one of filters 131-134 apply a filter to an audio signal received from path 101 representing an audio source. Filter 131 passes the filtered signal to amplifiers 141 and 145 which amplify the filtered signal. Filters 132-134 pass filtered signals to
25 other amplifiers as shown and each amplifier amplifies a respective filtered signal. Combiner 151 combines amplified signals received from amplifiers 141-144 and passes the resulting first output signal along path 161. Combiner 152 combines amplified signals received from amplifiers 145-148 and passes the resulting second output signal along path 163.

30 A location signal received from path 102 represents the desired apparent location of the source of the audio signal received from path 101. Position signals received from paths 162 and 164 represent position and/or orientation of one or more listeners. For example, the two position signals may represent position information for each ear of one listener or position information for two listeners. In the embodiment illustrated, respective gains of

- 10 -

amplifiers 141-144 in a first group of amplifiers are adapted in response to the location signal received from path 102 and the position signal received from path 162, and respective gains of amplifiers 145-148 in a second group of amplifiers are adapted in response to the location signal received from path 102 and the position signal received from path 164. In alternative embodiments, respective gains of amplifiers in a group of amplifiers may be adapted in response to only the location signal received from path 102 or only a respective position signal.

The multiple output signals may be used to provide binaural presentation to one or more listeners, monaural presentation to two or more listeners or a combination of binaural and monaural presentations. As explained above, the term "binaural" refers to presentations comprising two or more output signals.

The structure shown in Figure 2 implements HRTF for two output signals and can be extended to implement HRTF for additional output signals by adding a group of amplifiers for each additional output and coupling the input of each amplifier in a group to a respective filter. The illustrated structure comprises four filters but two or more filters may be used as desired.

Multiple Source and Output Signals

A functional block diagram shown in Figure 3 illustrates one structure of a device according to the teachings of the present invention which implements HRTF for multiple audio sources and multiple output signals. The structure and operation are substantially a combination of the structures and operations shown in Figures 1 and 2 and described above except that, preferably, the gains of amplifiers 141-148 are not adapted in response to location signals received from paths 102 and 104.

In an alternative embodiment discussed below, the respective gains of amplifiers 111-118 and/or amplifiers 141-148 may be adapted to effectively dedicate certain filters to particular audio sources and/or output signals to trade off accuracy of spatialization against numbers of sources and/or listeners.

Hybrid Structure

A functional block diagram shown in Figure 4 illustrates a hybrid filtering structure incorporated into a device according to the teachings of the present invention which implements a HRTF for one audio source and one output signal. Filter 3 and filter networks 21 and 22 each apply a filter to an audio signal received from path 101 representing an audio source. Filter 3 applies a filter having frequency response characteristics adapted by response control 10 in response to a location signal received

- 11 -

from path 102. Filter network 21 applies a filter having unvarying frequency response characteristics and utilizes an amplifier having a gain adapted by gain control 11 in response to the location signal received from path 102. Filter network 22 applies a filter having unvarying frequency response characteristics and utilizes an amplifier having a gain adapted by gain control 12 in response to the location signal received from path 102. The signals resulting from filter 3 and filter networks 21 and 22 are combined by combiner 151 and the resulting output signal is passed along path 161.

The location signal received from path 102 represents the desired apparent location of the source of the audio signal received from path 101. In an alternative embodiment, response control 10 and gain controls 11 and 12 may respond to other signals such as position signals representing position and/or orientation of a listener, and/or signals representing reflection effects.

As shown in Figures 5a and 5b, the filter networks may be implemented by an amplifier 111 with gain adapted in response to gain control 11 and a filter 131. In one embodiment, the input of the filter is coupled to the output of the amplifier. In another embodiment, the input of the amplifier is coupled to the output of the filter.

In one application, filter 3 implements a direct-path response function for one audio source to one ear of one listener and one or more filter networks synthesize the effects of reflections for one audio source to both ears of all listeners. Propagation effects on the reflected soundwaves, including delays, reflective- and transmissive-materials filtering, air absorption, soundfield spreading losses and source-aspect filtering, may be synthesized by delaying and filtering signals at various points in the structure but preferably at either the input or output of the filter networks. In many applications, reflections may be rendered with sufficient accuracy using as few as two or three filter networks.

In another application, reflections of one audio signal are spatialized for multiple output signals using only one set of filters having unvarying frequency response characteristics. Figure 6 illustrates a hybrid structure which synthesizes two reflected soundwaves for each of two output signals. The two output signals may be intended for binaural presentation to one listener or may be intended for monaural presentation to two listeners.

Referring to Figure 6, filter 3 generates a direct-path response along path 160 by applying a filter to an audio signal received from path 101. Filter 131 applies a filter to the audio signal and passes the filtered signal to amplifiers 141, 143, 145 and 147 which amplify the filtered signal. Filter 132 applies a filter to the audio signal and passes the

- 12 -

filtered signal to amplifiers 142, 144, 146 and 148 which amplify the filtered signal. Combiner 151 combines signals received from amplifiers 141 and 142 and passes the combined signal to delay element 171. Combiners 152-154 combine the signals received from the remaining amplifiers and pass the combined signals to respective delay elements 172-174. Combiner 155 combines delayed signals received from delay elements 171 and 172 and passes the resulting signal along path 161. Combiner 156 combines delayed signals received from delay elements 173 and 174 and passes the resulting signal along path 163. If a binaural presentation is desired, the signals passed along paths 160 and 161 are combined for presentation to one ear and the output from a second filter 3, not shown, is combined with the signal passed along path 163 for presentation to the second ear.

A location signal received from path 102 represents the desired apparent position of the source of the audio signal received from path 101. An ambient signal also received from path 102 represents the reflection geometry of the ambient environment. Position signals received from paths 162 and 164 represent position and/or orientation information for each ear of one listener or position information for two listeners. In the embodiment illustrated, filter 3 adapts frequency response characteristics in response to the location signal and, preferably, in response to the position signal for one listener. Respective gains of amplifiers 141-144 are adapted in response to the location signal and the ambient signal received from path 102 and the position signal received from path 162, and respective gains of amplifiers 145-148 are adapted in response to the location signal and the ambient signal received from path 102 and the position signal received from path 164. The gains of these amplifiers are adapted according to the direction of arrival for a reflected soundwave to be synthesized.

Delay elements 171 and 172 impose signal delays of a duration adapted in response to the location signal and the ambient signal received from path 102 and the position signal received from path 162. Delay elements 173 and 174 impose signal delays of a duration adapted in response to the location signal and the ambient signal received from path 102 and the position signal received from path 164. The durations of the respective delays are adapted according to the length of the propagation path of respective reflected soundwaves. In addition, filtering and/or amplification may be provided with the delays to synthesize various propagation and ambient effects such as those described above.

Additional amplifiers, combiners and delay elements may be incorporated into the illustrated embodiment to increase the number of synthesized reflected soundwaves and/or the number of output signals. These additional components do not significantly increase

the complexity of the HRTF because the number of filters used to synthesize reflections is unchanged.

Derivation of Filters

Efficiency of implementation may be achieved in each of the structures discussed above by utilizing an appropriate set of N filters having unvarying frequency response or, equivalently, unvarying impulse response characteristics. For discrete-time systems, these filters may be derived from an optimization process which derives an impulse response $q_j(t_p)$ for each filter in a set of N unit-energy filters that, when weighted and summed, form a composite impulse response $\hat{h}(\theta, \phi, t_p)$ providing the best approximation to each impulse response $h(\theta, \phi, t_p)$ in a set of M impulse responses. Preferably, the set H of M impulse responses represents an individual listener, real or imaginary, having localization characteristics which represent a large segment of the population of intended listeners. The set H of M impulse responses may be expressed as

$$H = \{h(\Theta_i, t_p)\} \quad \text{for } 0 \leq p < P \quad (1)$$

where Θ_i denotes a particular relative direction (θ, ϕ) ,

t_p denotes discrete sample times, and

P is the length of the impulse responses in samples.

Preferably, the angular spacing between adjacent directions is no more than 30 to 45 degrees in azimuth and 20 to 30 degrees in elevation. The composite impulse response $\hat{h}(\Theta_i, t)$ of the weighted and summed set of N filter impulse responses may be expressed as

$$\hat{h}(\Theta_i, t_p) = \sum_{j=0}^N w_j(\Theta_i) \cdot q_j(t_p) \quad (2)$$

where $w_j(\Theta_i)$ is the corresponding weight or coefficient for the impulse response of filter j at direction Θ_i .

The derivation process seeks to optimize the approximation by minimizing the square of the approximation error over all impulse responses in the set H , and may be expressed as

$$\frac{1}{P \cdot M} \|H - \hat{H}\|_F^2 = \frac{\sum_{i=0}^{M-1} \sum_{p=0}^{P-1} (h(\Theta_i, t_p) - \hat{h}(\Theta_i, t_p))^2}{P \cdot M} \quad \text{for } 0 < N < M \quad (3)$$

where $\|x\|_F$ denotes the Forbenious norm of x , and

\hat{H} is a set of M composite impulse responses $\hat{h}(\Theta_i, t_p)$.

According to expression 2, the set \hat{H} may be expressed as

$$\hat{H} = W \cdot Q \quad (4)$$

where W denotes an $N \times M$ matrix of coefficients $w_j(\theta_i)$, and

Q denotes a set of N impulse responses $q_j(t_p)$.

This decomposition allows the optimization of expression 3 to be expressed as

$$\min_{W, Q} (\|H - W \cdot Q\|_F) \quad (5)$$

By recognizing that the Forbenious norm is invariant under orthonormal transformation, it may be seen that the set of N impulse responses Q are the left singular vectors associated with the N largest singular values of H and that the coefficient matrix W is the product of the corresponding right singular vectors and diagonal matrix of singular values. The Forbenious norm of the approximation error is the sum of the $M-N$ smallest singular values.

The optimization process described above is known as "singular value decomposition" and derives a set of impulse responses $q_j(t_p)$ which are orthogonal. Additional information about singular value decomposition and the Forbenious norm may be obtained from Golub, et al., "Matrix Computations," Johns Hopkins University Press, 2nd ed., 1989, pp. 55-60, 70-78. Other decomposition processes and norms as such as those disclosed by Golub, et al. may be used to derive the W and Q matrices.

The choice of impulse response in the set H affects the resultant filters Q . For example, filters for use in a display providing only azimuthal localization may be derived from a set of impulse responses for directions which lie only in the horizontal plane. Similarly, filters for use in a display in which azimuthal localization is much more important than elevation localization may be derived from a set H which comprises many more impulse responses for directions in the horizontal plane than for directions above or below the horizontal plane. The set H may comprise impulse responses for a single ear or for both ears of one individual or of more than one individual. It should be understood, however, that as the number of impulse responses in the set H increases, the number of impulse responses in the set Q must also increase to achieve a given level of approximation error.

As another example, a set of filters which optimize only the magnitude response of HRTF may be derived from a set H which comprises linear- or minimum-phase impulse responses, or impulse responses which are time aligned in some manner. The phase response may be synthesized separately by ITD, discussed below.

- 15 -

The optimization process described above assumes that the impulse responses $q_j(t_p)$ in set H correspond to HRTF comprising both directionally-dependent aspects and directionally-independent aspects such as ear canal resonance. The process may also derive filters from impulse responses corresponding to other ATF such as DTF, for example, from which a common characteristic has been removed. The derived filters, taken together, approximate the ATF and the common characteristic excluded from the optimization may be provided by a separate filter. This is illustrated in Figures 7a and 7b.

Referring to Figure 7a, amplifier network 20 amplifies and combines the audio signals received from paths 101 and 103 to generate a set of intermediate signals which are passed to the set of N filters 131-134 derived by the optimization process, each of filters 131-134 applies a filter to a respective intermediate signal, combiner 151 combines the filtered signals to generate a composite signal, and filter 130 generates an output signal along path 161 by applying a filter having the common characteristics excluded from filters 131-134 to the composite signal. This structure corresponds to the structure illustrated in Figure 1 and is preferred in applications where the number of audio signals exceeds the number of output signals.

Referring to Figure 7b, filter 130 generates an intermediate signal by applying a filter having the common characteristics excluded from filters 131-134 to the audio signal received from path 101, the set of N filters 131-134 derived by the optimization process each filter the intermediate signal received from filter 130, and amplifier network 40 amplifies and combines the filtered signals to generate output signals along paths 161 and 163. This structure corresponds to the structure illustrated in Figure 2 and is preferred in applications where the number of output signals exceeds the number of audio signals.

It may be of interest to note that if the common characteristic excluded from the optimization process corresponds to the directionally-independent aspects of HRTF, then the first derived impulse response $\hat{h}(\Theta_i, t_p)$ is substantially equal to the Dirac delta function.

As mentioned above, the number of filters required to achieve a given approximation error depends on the impulse responses constituting the set H . Preferably, a set of linear- or minimum-phase impulse responses are used because the approximation error is expected to decrease more rapidly for increasing N than would occur for impulse responses including ITD which are not aligned in time with one another.

An acoustic display incorporating a set of filters and weights derived according to the process described above can spatialize an audio signal to any given direction Θ_k by calculating a set of weights $w_j(\Theta_k)$ appropriate for the given direction and using the weights

- 16 -

to set amplifier gains. The weights for a given direction can be calculated by linearly interpolating between weights $w_j(\theta_i)$ corresponding to the directions θ_i closest to the given direction.

In concept, each filter convolves a time-domain signal with a respective impulse response. Filtering may be accomplished in a variety of ways including recursive or so called infinite impulse response (IIR) filters, nonrecursive or so called finite impulse response (FIR) filters, lattice filters, or block transforms. No particular filtering technique is critical to the practice of the present invention; however, it is important to note that the composite filter response actually achieved from a filter implemented according to expression 2 may not match the desired composite impulse response derived by optimization. In preferred embodiments, the filters are checked to ensure that the difference between the desired impulse response and the actual impulse response is small. This check must take into account both magnitude and phase; therefore, the technique used to implement the filters must either preserve phase or otherwise account for changes in phase so that correct results are obtained from the weighted sum of the impulse responses.

Dynamic Reconfiguration

The function performed by the structure illustrated in Figure 3 may be expressed in algebraic form as

$$P(t_p) = W_{out}(\theta) \cdot Q \cdot W_{in}(\theta) \cdot S(t_p) \quad (6)$$

where $P(t_p)$ denotes a column vector of output signals of length L_{out} .

$S(t_p)$ denotes a column vector of input signals of length L_{in} .

$W_{in}(\theta)$ denotes an $M \times L_{in}$ matrix of input coefficients.

$W_{out}(\theta)$ denotes an $L_{out} \times M$ matrix of output coefficients, and

Q denotes an $M \times M$ diagonal matrix of filters.

This structure may implement HRTF for each input signal and output signal provided the matrix product $W_{out}(\theta) \cdot Q \cdot W_{in}(\theta)$ can be made to approximate the source-listener HRTF matrix. This approximation can be made if the matrix product is full rank.

If only one input signal is present, L_{in} equals one, the rank of matrix W_{in} equals one, and the matrix product may be rewritten as shown in the following expression:

$$X_{out}(\theta) \cdot Q \quad (7a)$$

where $X_{out}(\theta)$ denotes an $L_{out} \times M$ matrix. This condition results in a structure which is equivalent to the structure illustrated in Figure 2. If only one output signal is needed, L_{out} equals one, the rank of W_{out} equals one, and the matrix product may be rewritten as shown in the following expression:

$$Q \cdot X_L(\theta) \quad (7b)$$

where $X_L(\theta)$ denotes an $M \times L_m$ matrix. This condition results in a structure which is equivalent to the structure illustrated in Figure 1. If the minimum rank of matrices W_m and W_{out} is K , however, the matrix product in expression 6 can be rewritten in a form shown in expressions 7a or 7b if K sets of filters Q are available; however, if only $J < K$ sets of filters Q are available, then a rank J approximation of the rank K system may be used but spatialization performance will be degraded.

Referring to the structure illustrated in Figure 3, for example, the filters may be configured into one set of four filters, two sets of two filters, four sets of one filter, or three sets each comprising either one or two filters. When configured as one set of four filters, the structure may implement HRTF for one source signal and any number of output signals, as shown in Figure 2, or it may implement HRTF for any number of input signals and one output signal, as shown in Figure 1. When configured as two sets of filters, the structure may implement HRTF for two source signals and any number of output signals or for any number of input signals and two output signals. Reconfiguration may be accomplished by setting the gains in various amplifiers to zero, thereby isolating the filters from certain input signals or from certain output signals.

Dynamic reconfiguration is useful in applications which must support a widely varying number of sources and listeners because a device of given complexity may easily trade off the accuracy of spatialization against the smaller of the number of input signals and output signals. Accuracy of spatialization can sometimes be sacrificed without noticeable effect when listener ability to localize is degraded. Such degradation occurs, for example, when listeners are distracted, overwhelmed by very large numbers of sound sources, or when a sound is difficult to localize. Examples of sounds which are difficult to localize are those generated by narrow-band or quiet short-duration signals, sounds which occur in a reverberant environment, or sounds which originate in particular regions such as directly overhead or at great distances from the listener.

Variations and Extensions

In preferred embodiments, the magnitude of HRTF response is implemented by linear- or minimum-phase filters and the phase of HRTF response is implemented by delays. Relative delays between left- and right-ear signals produce ITD which is an important azimuth cue. Delays may also be used to synthesize the arrival of reflections or to simulate the effects of distance. Filtering and scaling may be used to synthesize propagation and ambient effects such as air absorption, soundfield spreading losses,

nonuniform source radiation patterns, and transmissive- and reflective-materials characteristics. This additional processing may be introduced in a wide variety of places. Although no particular implementation is critical to the practice of the present invention, some implementations are preferred. Preferably, delays, filtering and scaling are
5 introduced at points in an embodiment which reduces implementation costs. Processing unique to each source is preferably provided for the audio signal prior to amplification and filtering. Processing unique to each output signal is preferably provided for the output signal after filtering, amplification and combining.

Throughout this discussion, reference is made to listener position and/or orientation.
10 Orientation refers to the orientation of the head relative to the audio source location. Position, as distinguished from orientation, refers to the relative location of the source and the center of the head. Listener position and/or orientation may be obtained using a wide variety of techniques including mechanical, optical, infrared, ultrasound, magnetic and radio-frequency techniques, and no particular way is critical to the practice of the present
15 invention.

Listener position and/or orientation may be sensed using headtracking systems such as the Bird magnetic sensor manufactured by Ascension Technology Corporation, Burlington, Vermont, or the six-degree-of-freedom ISOTRAK II™, InsideTRAK™ and FASTRAK™ sensors manufactured by Polhemus Corporation, Colchester, Vermont.

20 The position and orientation of a listener riding in a vehicle may also be sensed by using mechanical, magnetic or optical switches to sense vehicle location and orientation. This technique is useful for amusement or theme park rides in which listeners are transported along a track in capsules or other vehicles.

The position and orientation of a listener may be sensed from static information
25 incorporated into the acoustic display. For example, position and orientation of listeners seated in a motion picture theater or seated around a conference table may be presumed from information describing the theater or table geometry.

Amplifier gain and/or time delays may be adapted to synthesize ambient effects in response to signals describing the simulated environment. Longer delays may be used to
30 simulate the reverberance of larger rooms or concert halls, or to simulate echoes from distant structures. Highly reflective acoustic environments may be simulated by incorporating a large number of reflections with increased gain for late reflections. The perception of distance from the audio source can be strengthened by controlling the relative gain for reflected soundwaves and direct path soundwaves. In particular, the delay and

direction of arrival of reflected soundwaves may be synthesized using information describing the geometry and acoustical properties of reflective surfaces, and position and/or orientation of a listener within the environment.

- 5 Amplifier gain and/or time delays may also be adapted to adjust HRTF responses to individual listener localization characteristics. ITD may be adjusted to account for variations in head size and shape. Amplifier gain may be adapted to adjust spectral shaping to account for size and shape of head and ear pinnae. In one embodiment of an acoustic display, a listener cycles through different coefficient matrices W while listening to the spatial effects and selects the matrix which provides the most desirable spatialization.

- 20 -

CLAIMS

1. A method for providing an acoustic display of aural information conveying apparent location, said method comprising the steps of:

5 receiving one or more audio signals and one or more location signals representing one or more sources of aural information, wherein said location signals represent apparent locations for said sources,

 generating one or more first signals by applying a first network to said one or more audio signals,

10 generating a plurality of filtered signals by applying a plurality of filters to said one or more first signals, and

 generating one or more output signals by applying a second network to said filtered signals,

wherein

15 a) said first signals are generated by applying a plurality of first amplifiers to said one or more audio signals, each of said first amplifiers having a respective gain adapted in response to said one or more location signals,

and/or

 b) said second signals are generated by applying a plurality of second amplifiers to said filtered signals, each of said second amplifiers having a respective gain adapted in response to said one or more location signals.

2. A method according to claim 1 wherein said first network comprises two or more groups of first amplifiers and a respective first signal is generated from the output of a
25 respective group of first amplifiers, a respective first amplifier in each group amplifying one of said audio signals.

3. A method according to claim 1 or 2 wherein said second network combines two or more of said filtered signals to generate a respective output signal.

30

4. A method according to any one of claims 1 through 3 which further comprises delaying at least one of said plurality of first signals, the amount of delay adapted in response to said one or more location signals and/or a signal representing aural localization characteristics of a listener.

35

- 21 -

5. A method according to claim 1 wherein said second network comprises two or more groups of second amplifiers and a respective output signal is generated by combining the output of a respective group of second amplifiers, a respective second amplifier in each group amplifying the filtered signal generated by a respective one of said plurality of filters.

5

6. A method according to claim 1 or 5 wherein said first network conveys each of said audio signals substantially without change as one or more of said first signals.

7. A method according to any one of claims 1 through 6 which further comprises
10 delaying at least one of said output signals, the amount of delay adapted in response to said one or more location signals and/or a signal representing aural localization characteristics of a listener.

8. A method according to any one of claims 1 through 7 wherein one or more of said
15 respective gains are adapted in response to a signal representing aural localization characteristics of a listener.

9. A method according to any one of claims 1 through 8 wherein, in response to a configuration signal, said first network and/or said second network are adapted to configure
20 said plurality of filters into one or more sets of filters, thereby providing for a variable number of audio signals and/or a variable number of output signals.

10. A method for providing an acoustic display of aural information conveying apparent location, said method comprising the steps of:

25 receiving an audio signal representing said aural information and receiving a location signal representing an apparent location for a source of said aural information, generating a first filtered signal by applying a first filter to said audio signal, said first filter having variable frequency response characteristics adapted in response to said location signal,

30 generating one or more second filtered signals by applying a respective network to said audio signal, each network comprising one or more second filters and one or more amplifiers, each second filter having a respective unvarying frequency response characteristic and each amplifier having a respective gain adapted in response to said location signal, and

- 22 -

generating an output signal by combining said first filtered signal and said one or more second filtered signals.

5 11. A method according to claim 10 wherein a respective one of said second filtered signals is generated by applying a respective second filter to said audio signal and by amplifying the output of said respective second filter using a respective one of said one or more amplifiers.

10 12. A method according to claim 10 or 11 which further comprises delaying at least one of said second filtered signals, the amount of delay adapted in response to said location signal and/or a signal representing aural localization characteristics of a listener.

15 13. A method according to any one of claims 10 through 12 wherein said variable frequency response characteristics and/or said respective gains are adapted in response to a signal representing aural localization characteristics of a listener.

20 14. A method according to any one of claims 1 through 13 wherein one or more of said respective gains are adapted in response to a position signal indicating the position of a listener.

15. A method according to any one of claims 1 through 14 wherein one or more of said respective gains are adapted in response to a signal representing ambient characteristics.

25 16. A method according to any one of claims 1 through 15 wherein said plurality of filters have impulse responses which are substantially mutually orthogonal.

17. A method according to claim 16 wherein said impulse responses are derived by singular value decomposition of a given set of impulse responses.

30 18. An apparatus for providing an acoustic display of aural information conveying apparent location, said apparatus comprising:

means for receiving one or more audio signals and one or more location signals representing one or more sources of aural information, wherein said location signals represent apparent locations for said sources,

- 23 -

means for generating one or more first signals by applying a first network of a plurality of first amplifiers to said one or more audio signals, each of said first amplifiers having a respective gain adapted in response to said one or more location signals,

5 means for generating a plurality of filtered signals by applying a plurality of filters to said one or more first signals, and

 means for generating one or more output signals by applying a second network to said filtered signals.

10 19. An apparatus according to claim 18 wherein said first network comprises two or more groups of first amplifiers and a respective first signal is generated from the output of a respective group of first amplifiers, a respective first amplifier in each group amplifying one of said audio signals.

15 20. An apparatus according to claim 18 or 19 wherein said second network combines two or more of said filtered signals to generate a respective output signal.

20 21. An apparatus according to any one of claims 18 through 20 which further comprises means for delaying at least one of said plurality of first signals, the amount of delay adapted in response to said one or more location signals and/or a signal representing aural localization characteristics of a listener.

 22. An apparatus for providing an acoustic display of aural information conveying apparent location, said apparatus comprising:

25 means for receiving one or more audio signals and one or more location signals representing one or more sources of aural information, wherein said location signals represent apparent locations for said sources,

 means for generating one or more first signals by applying a first network to said one or more audio signals,

30 means for generating a plurality of filtered signals by applying a plurality of filters to said one or more first signals, and

 means for generating one or more output signals by applying a second network of a plurality of second amplifiers to said filtered signals, each of said second

- 24 -

amplifiers having a respective gain adapted in response to said one or more location signals.

23. An apparatus according to claim 22 wherein said second network comprises two
5 or more groups of second amplifiers and a respective output signal is generated by combining the output of a respective group of second amplifiers, a respective second amplifier in each group amplifying the filtered signal generated by a respective one of said plurality of filters.

24. An apparatus according to claim 22 or 23 wherein said first network conveys each
10 of said audio signals substantially without change as one or more of said first signals.

25. An apparatus according to any one of claims 22 through 24 which further comprises means for delaying at least one of said output signals, the amount of delay adapted in response to said one or more location signals and/or a signal representing aural localization
15 characteristics of a listener.

26. An apparatus according to any one of claims 18 through 25 wherein one or more of said respective gains are adapted in response to a signal representing aural localization characteristics of a listener.
20

27. An apparatus according to any one of claims 18 through 26 further comprising means for adapting, in response to a configuration signal, said first network and/or said second network to configure said plurality of filters into one or more sets of filters, thereby providing for a variable number of audio signals and/or a variable number of output signals.
25

28. An apparatus for providing an acoustic display of aural information conveying apparent location, said apparatus comprising:

means for receiving an audio signal representing said aural information and receiving a location signal representing an apparent location for a source of said aural
30 information,

means for generating a first filtered signal by applying a first filter to said audio signal, said first filter having variable frequency response characteristics adapted in response to said location signal,

means for generating one or more second filtered signals by applying a
35 respective network to said audio signal, each network comprising one or more second

- 25 -

filters and one or more amplifiers, each second filter having a respective unvarying frequency response characteristic and each amplifier having a respective gain adapted in response to said location signal, and

means for generating an output signal by combining said first filtered signal and said one or more second filtered signals.

29. An apparatus according to claim 28 wherein a respective one of said second filtered signals is generated by applying a respective second filter to said audio signal and by amplifying the output of said respective second filter using a respective one of said one or more amplifiers.

30. An apparatus according to claim 28 or 29 which further comprises means for delaying at least one of said second filtered signals, the amount of delay adapted in response to said location signal and/or a signal representing aural localization characteristics of a listener.

31. An apparatus according to any one of claims 28 through 30 wherein said variable frequency response characteristics and/or said respective gains are adapted in response to a signal representing aural localization characteristics of a listener.

32. An apparatus according to any one of claims 18 through 31 wherein one or more of said respective gains are adapted in response to a position signal indicating the position of a listener.

33. An apparatus according to any one of claims 18 through 32 wherein one or more of said respective gains are adapted in response to a signal representing ambient characteristics.

34. An apparatus according to any one of claims 18 through 33 wherein said plurality of filters have impulse responses which are substantially mutually orthogonal.

35. An apparatus according to claim 34 wherein said impulse responses are derived by singular value decomposition of a given set of impulse responses.

//

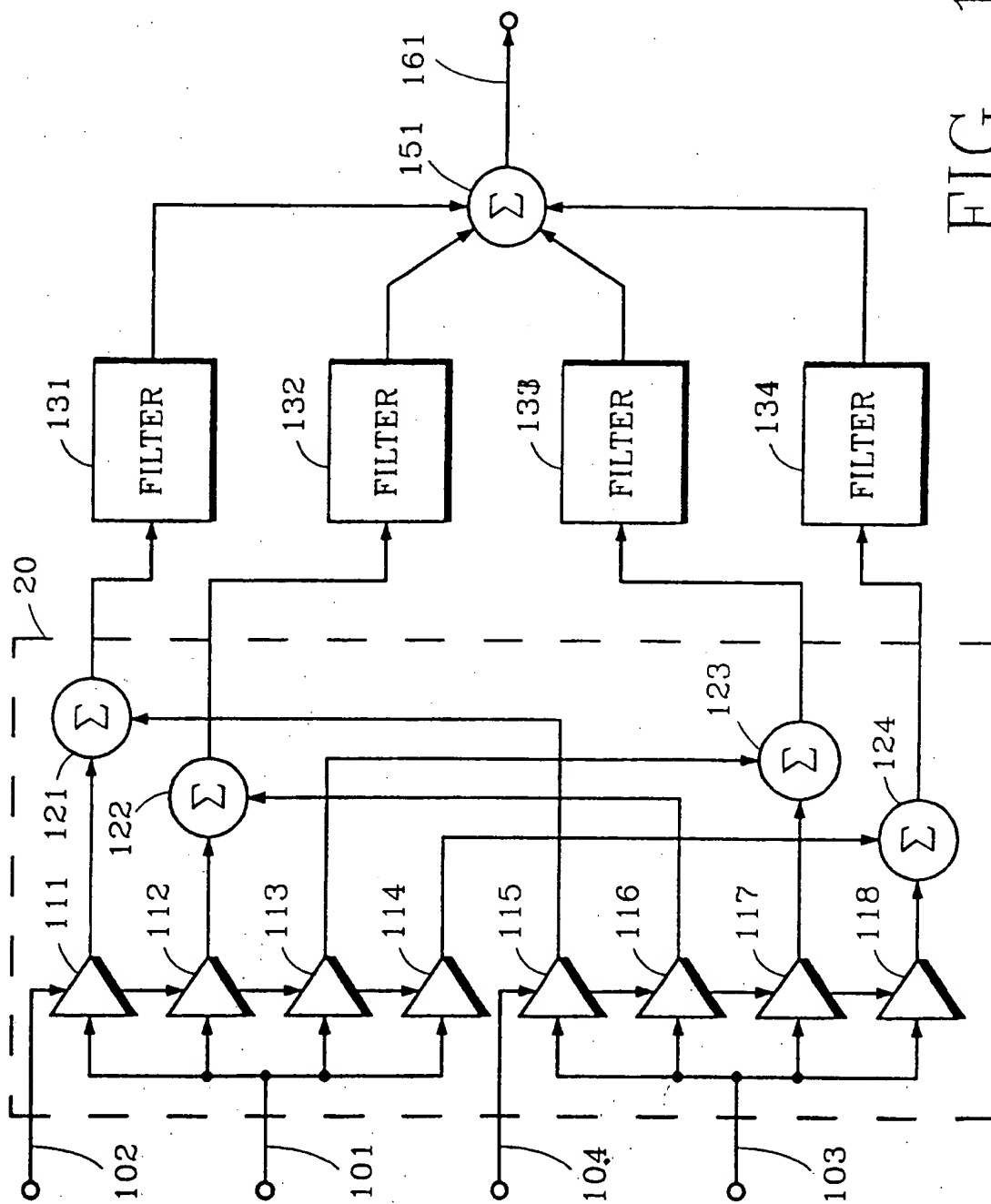


FIG. 1

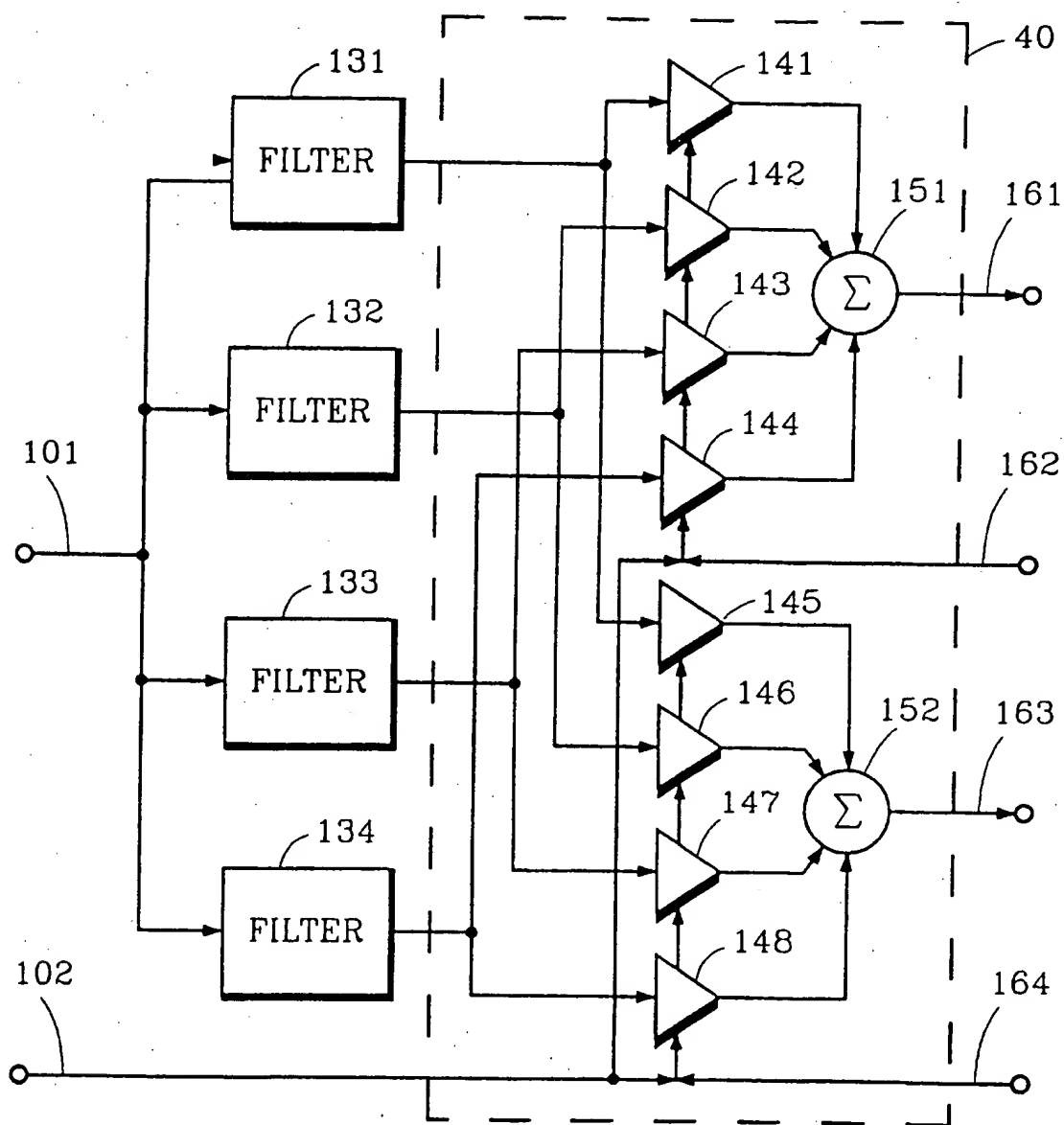


FIG. 2.

3 / 6

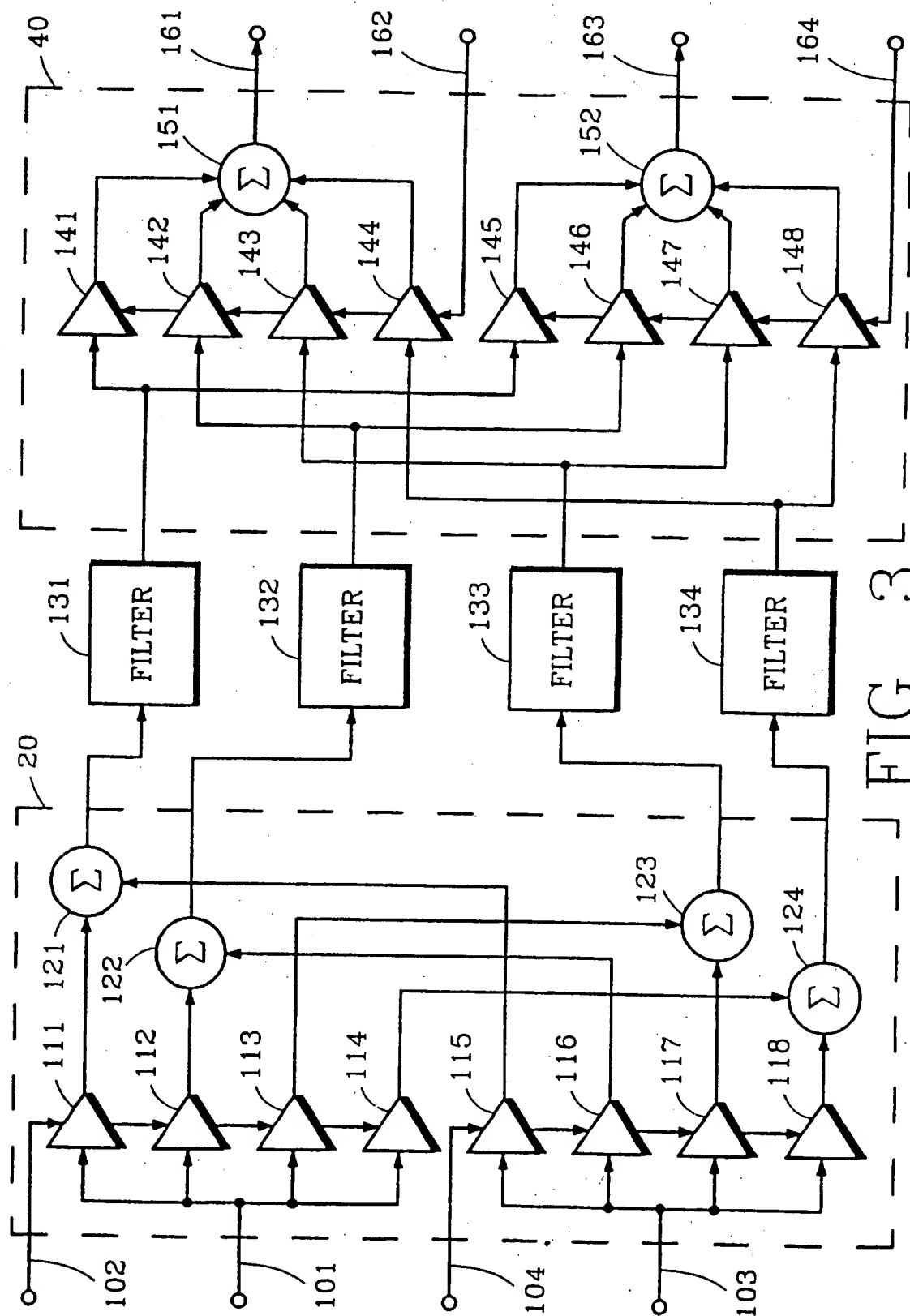


FIG. 3

4 / 6

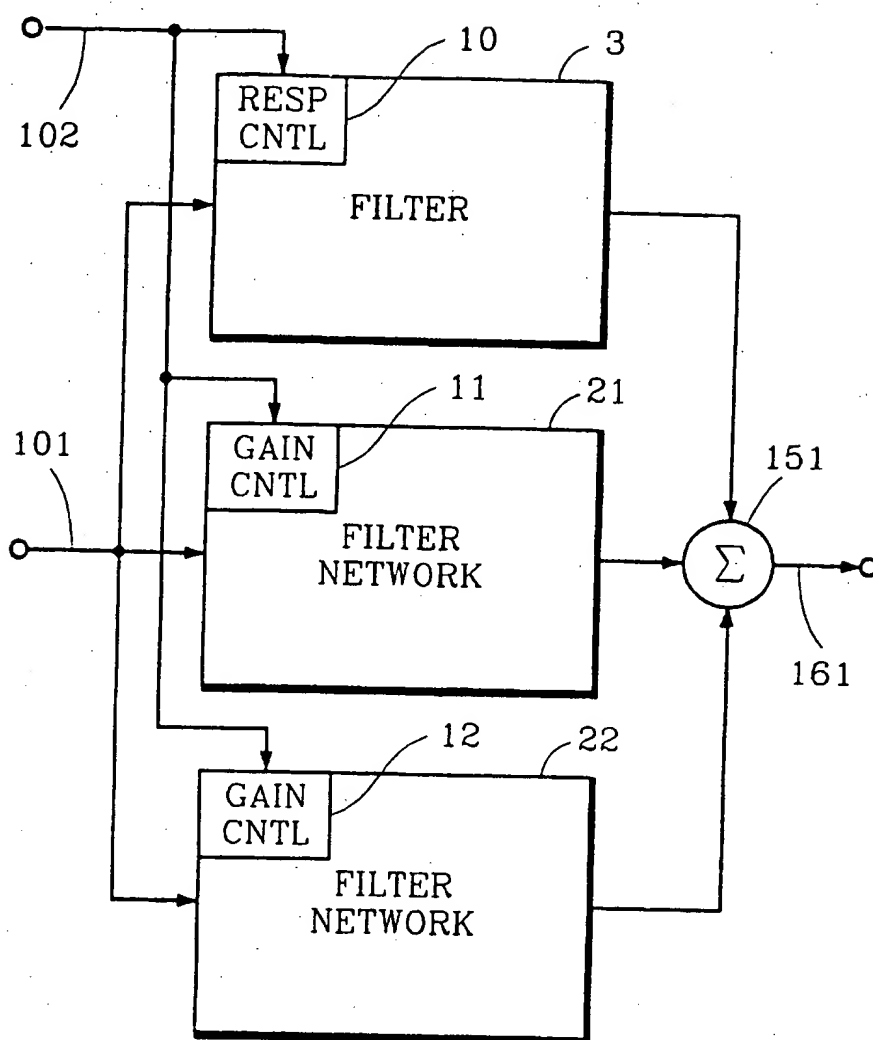


FIG. 4

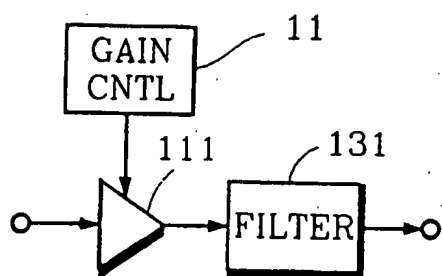


FIG. 5a

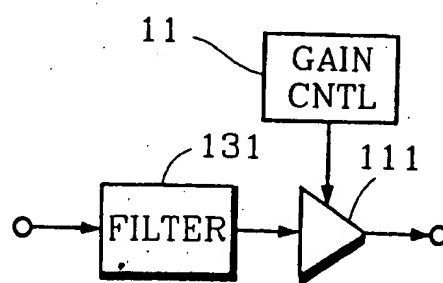


FIG. 5b

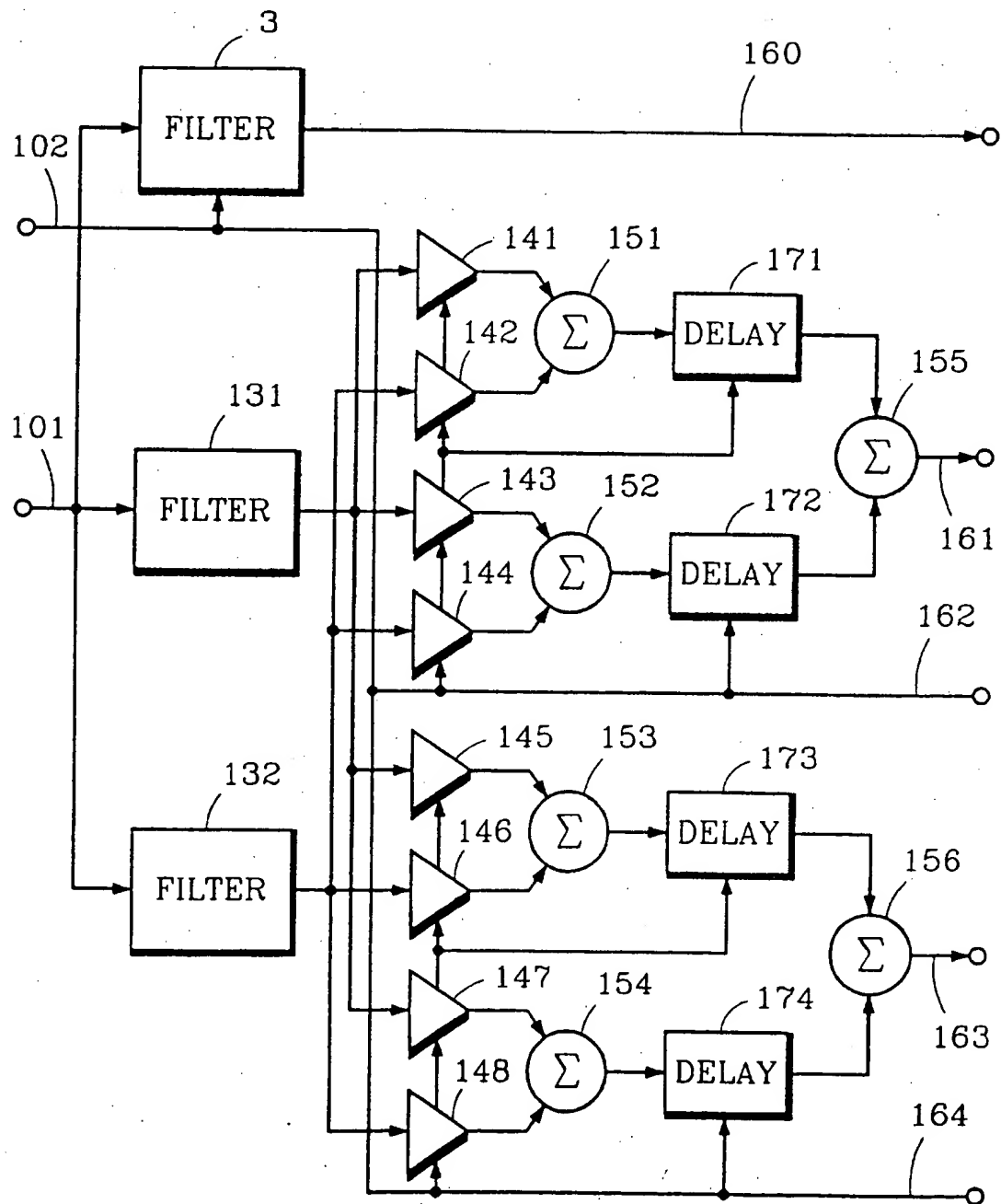


FIG. 6

6/6

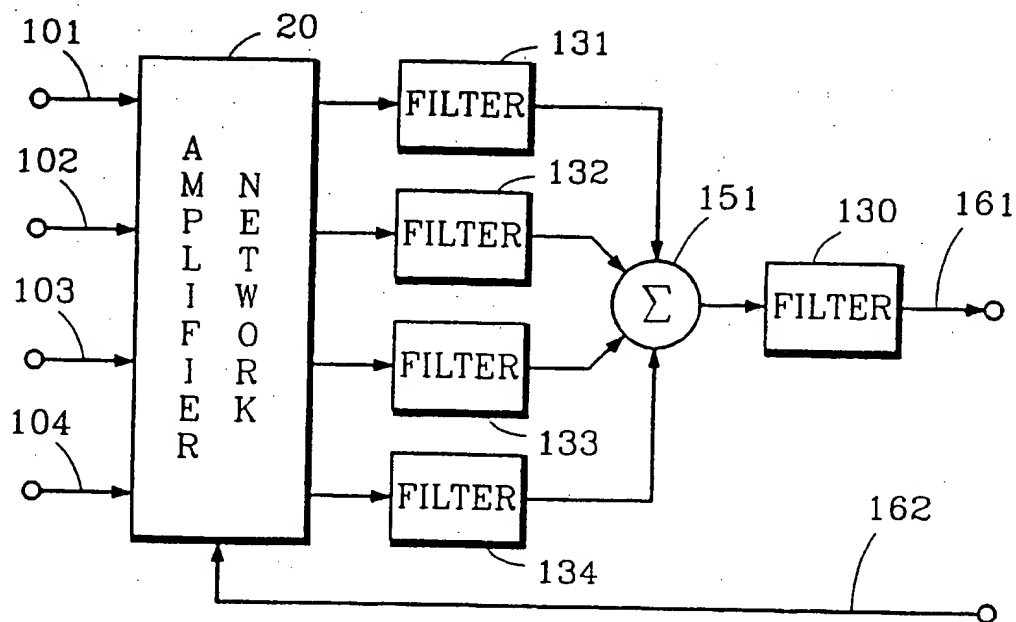


FIG. 7a

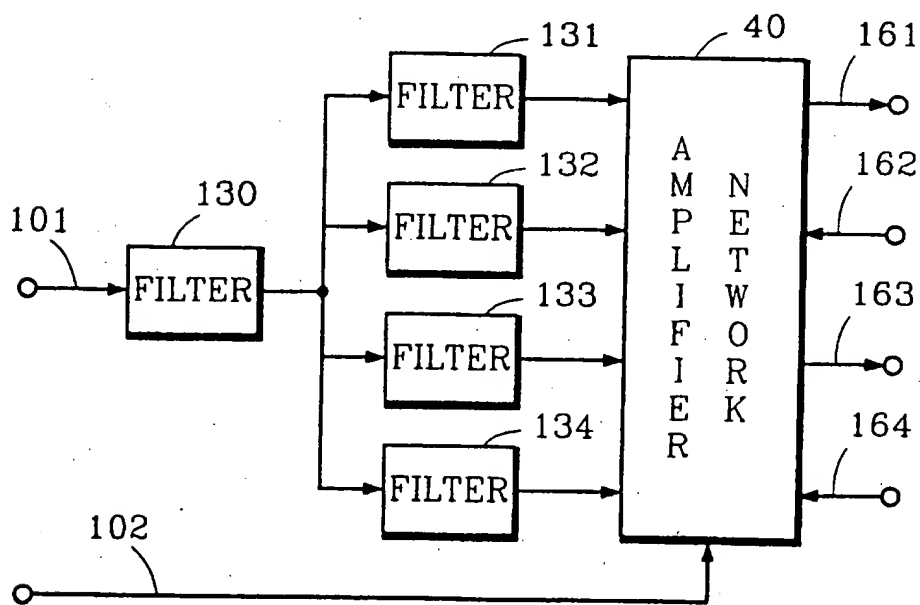


FIG. 7b

INTERNATIONAL SEARCH REPORT

International Application No.
PCT/US 95/13874

A. CLASSIFICATION OF SUBJECT MATTER
IPC 6 H04S5/00

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 6 H04S H04B H04L

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	GB,A,2 238 936 (QSOUND) 12 June 1991 see page 1, line 1-5 see page 9, line 16 - page 15, line 7 ---	1-3,5,6, 9-11, 18-20, 22-24, 27-29
A	EP,A,0 142 213 (PHILIPS) 22 May 1985 see page 6, line 15 - page 11, line 20 --- -/--	1,2,4-7, 10,12, 18-25, 28,30

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

* Special categories of cited documents:

- *A* document defining the general state of the art which is not considered to be of particular relevance
- *E* earlier document but published on or after the international filing date
- *L* document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- *O* document referring to an oral disclosure, use, exhibition or other means
- *P* document published prior to the international filing date but later than the priority date claimed

T later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

X document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

Y document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

A document member of the same patent family

Date of the actual completion of the international search

27 February 1996

Date of mailing of the international search report

10.04.96

Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2
NL - 2280 HV Rijswijk
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,
Fax: (+31-70) 340-3016

Authorized officer

Zanti, P

INTERNATIONAL SEARCH REPORT

International Application No.

PCT/US 95/13874

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	<p>EP,A,0 357 402 (Q SOUND) 7 March 1990</p> <p>see page 2, line 31-38 see page 3, line 51 - page 5, line 31 see page 5, line 56 - page 7, line 7 ---</p>	<p>1,4,7,8, 10, 12-15, 18,21, 22,25, 26,28, 30-33</p>
A	<p>EP,A,0 448 758 (STANDARD ELEKTRIK LORENTZ) 2 October 1991</p> <p>see page 2, line 46-50 see page 3, line 54 - page 5, line 11 -----</p>	<p>1,10, 16-18, 22,28, 34,35</p>

INTERNATIONAL SEARCH REPORT

Information on patent family members

International Publication No
PCT/US 95/13874

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
GB-A-2238936	12-06-91	US-A- 5138660	11-08-92
		US-A- 5026051	25-06-91
		US-A- 5052685	01-10-91
		AU-B- 625530	16-07-92
		AU-B- 6779790	13-06-91
		BG-A- 51469	14-05-93
		CA-A- 2031665	08-06-91
		EP-A- 0499729	26-08-92
		IL-A- 96553	12-04-94
		JP-A- 4242684	31-08-92
		PL-B- 165355	30-12-94
		CN-A,B 1053163	17-07-91
EP-A-142213	22-05-85	NL-A- 8303945	17-06-85
		AU-B- 572227	05-05-88
		AU-B- 3561584	23-05-85
		CA-A- 1227756	06-10-87
		DE-A- 3469981	21-04-88
		JP-A- 60167600	30-08-85
		US-A- 4625326	25-11-86
EP-A-357402	07-03-90	US-A- 5046097	03-09-91
		AT-T- 123369	15-06-95
		AU-B- 621655	19-03-92
		AU-B- 4100089	08-03-90
		BG-B- 60225	30-12-93
		CA-A- 1329911	31-05-94
		DE-D- 68922885	06-07-95
		DE-T- 68922885	12-10-95
		IL-A- 91464	28-11-94
		JP-A- 2298200	10-12-90
		NO-B- 175229	06-06-94
		PL-B- 163716	29-04-94
		US-A- 5208860	04-05-93
		CN-A- 1050119	20-03-91
		US-A- 5105462	14-04-92
EP-A-448758	02-10-91	AT-T- 125090	15-07-95
		CA-A- 2038653	29-09-91
		CA-C- 2038653	20-09-94

